

FIELD MEASUREMENTS, WEB PROCEDURES, AND ONLINE TOOLS FOR ASSESSING OCCUPATIONAL EXPOSURE TO NON-IONIZING RADIATION

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CNR-IFAC

The Institute of Applied Physics "Nello Carrara" (IFAC) was established in March 2002 in Florence (previously IROE, Research Institute on Electromagnetic Waves).

IFAC has expertise in physical investigation methods for the development of devices and instruments, mathematical and computer methods for modeling and processing of data and images, with applications in:

- space, aerospace, and earth observation
- health, nanomedicine, and safety
- environmental monitoring and food quality
- cultural heritage





BRIC 2017-2025

- Collaborative Research Calls funded by INAIL (National Institute for Insurance against Accidents at Work)
- Involving several Italian institutions:
 - CNR-IFAC ("Nello Carrara" Institute for Applied Physics of the Italian National Research Council, Florence)
 - CNR-IFC Pisa
 - ISS (Italian National Institute of Health)
 - USL Siena
 - Policlinico San Matteo
 - University of Modena and Reggio Emilia



BRIC 2017-2025

- Activities focused on professional exposure related to AIMD (Active Implantable and Wearable Medical Devices) wearers
- Current project: Risk assessment and management deriving from exposure to new sources of electromagnetic fields for the protection of workers with active implantable medical devices



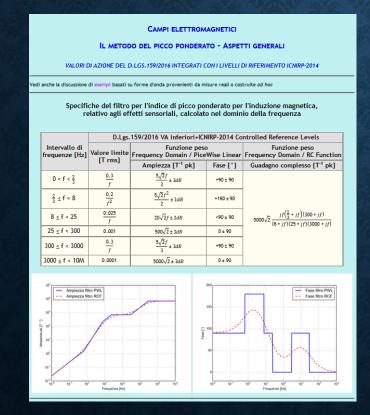
- Web tools for the assessment of occupational exposure to Non Ionizing Radiation
- Web portal: https://webnir.eu
- 3 sections:
 - EMF (ElectroMagnetic Fields)
 - AIMD (Active Implantable and Wearable Medical Devices)
 - AOR (Artificial Optical Radiation)
- Updated with new technologies and implementation of new technical features (responsive site, multilingual, keyword search): https://webnir2.ifac.cnr.it (switching off soon)

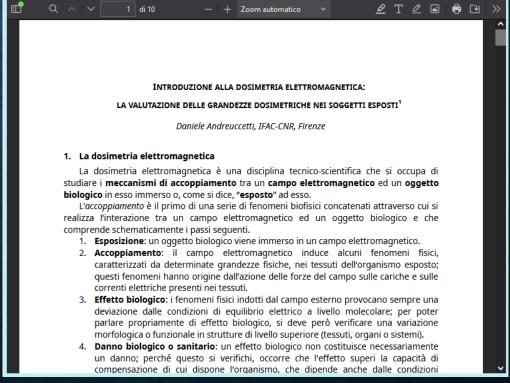


WEBNIR

It makes available:

Technical documents (web pages or PDFs)



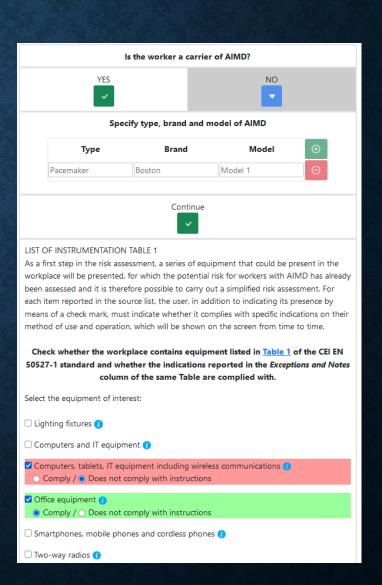




It makes available:

- Technical documents (web pages or PDFs)
- Interactive procedures

A backend interface allows the admin to insert data, automatically making available a frontend where the user can answer questions following a path according to the procedure.





WEBNIR

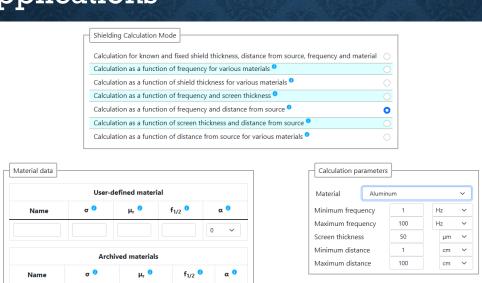
It makes available:

Technical documents (web pages or PDFs)

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1.000022

- Interactive procedures
- Calculation applications

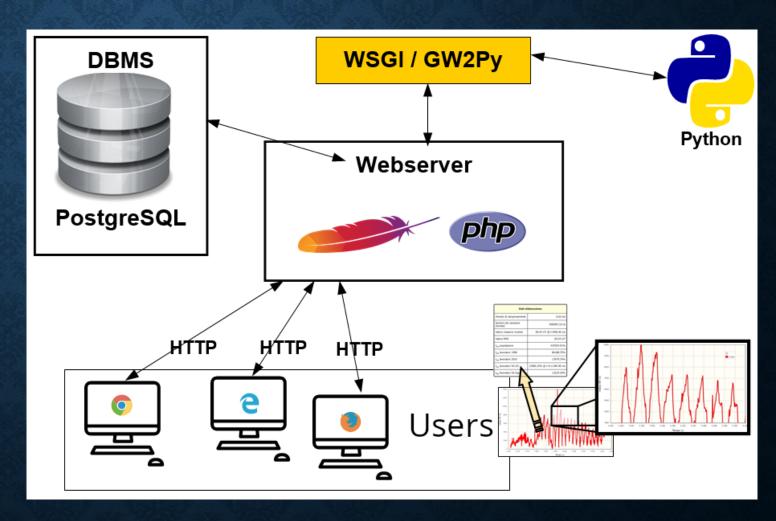


Definizione della struttura	dei sistemi di condutt	tori		
Numero di sistemi 1 3				
Tanks of sales in				
1				
Parametri generali della struttura n. 1				
Nome della struttura	Struttura n. 1			
Altezza da terra del condu	ttore più basso	20 0 m		
Distanza dall'origine, lung	o il terreno	10.0 0 m		
Utilizzo facoltativo di sos	tegni a massimo impa	atto •		
Tensione efficace nominal	e tra le fasi 132 ki	v ~		
Agrapa	in the	139	19 19	
l W		1 300	200	
Parametri dei conduttori	della struttura n. 1			
N. conduttori nella struttu	ra (fino a 30)	3 0		
X (m) **	Y (m) 🍮	I (A)	Fase (°)	
-7.1	0 0	300 ○	0 0	
0 0	0 0	300 €	120 0	
7.1 0	0 0	300 0	240 0	
Replica questi parametri a	la struttura n	v 3		
Replica questi parametri a	la struttura n	× >		
Replica questi parametri a	la struttura n	·		
	la struttura n	o di terra		
		o di terra	rreno 1.5	© m
Posizione dei punti d	i calcolo lungo il pian			© m
Posizione dei punti d Distanza iniziale ⁶	i calcolo lungo il pian	Altezza sul te		
Posizione dei punti d Distanza iniziale Passo Numero di punti	calcolo lungo il piano -100.00 m 1.0 0 m 200 0	Altezza sul te		
Posizione dei punti d Distanza iniziale Passo	calcolo lungo il piano -100.00 m 1.0 0 m 200 0	Altezza sul te	terreno 0	0



THE COMMUNICATION PROTOCOL

- The tools have a user interface created via a web page
- The computational load is split between the user's computer and the server platform
- Gw2Py: POST data to server, get data from server
- JSON as a standard format for data exchange





EMF TOOLS

- General aspects
 - Consultation and comparison of regulatory limits
 - Interpolation of index measurements and calculation of the compliance distance with determination of the uncertainty
- Characterization of sources in the external environment
 - Calculation of the electric field generated by systems of indefinite rectilinear conductors
- Processing of data files from exposure measurements
 - Calculation of weighted peak indices for low and intermediate frequency magnetic field sources
 - Motion in a Static Magnetic Field Processing of Perceived Magnetic Field Measurements
 - · Loading, recognition, and processing of measurement data files in the time or frequency domain
- Applications to support the reduction to compliance
 - Comparison of the electric field generated by systems of indefinite rectilinear conductors
 - Calculating the shielding effectiveness of an ideal screen



Regulations list Regulations comparison Regulations filter Instructions	
ICNIRP Guidelines 1994 (Static magnetic fields)	~
ICNIRP Guidelines 1998 (EMF up to 300 GHz)	
ICNIRP Guidelines 2009 (Static magnetic fields)	
ICNIRP Guidelines 2010 (LF)	
ICNIRP Guidelines 2014 (Movement in a static magnetic field)	
Raccomandazione 1999/519/CE	
Direttiva 2013/35/UE	~
ICNIRP Guidelines 2014 + Direttiva 2013/35/UE	~
ICNIRP Guidelines 2020 (100 kHz to 300 GHz)	~

- Tab system
- Regulations grouped by document (ICNIRP guidelines...)



ICNIRP Guidelines 2009 (Static magnetic fields)

ICNIRP. Guidelines on limits of exposure to static magnetic fields. Health Physics, Vol.96, N.4, April 2009, pp.504-514.

Download PDF: [INT] [EXT]

Code	Full name	
ICNIRP2009BSTAT	ICNIRP Guidelines 2009 - Exposure limits for static magnetic fields	Details 🔍

 Limits not dependent on frequency are displayed in a table

Short name	ICNIRP-2009 B-Stat	
Туре	Exposure limits	Restriction
Quantity	Magnetic flux density	Occupational ex
Metric	Static field or DC value	•
Subject	Population and workers	Occupational ex movement, spa
Effect	Undifferentiated	Occupational ex
Level	Undifferentiated	Population expo
Localization	Whole body exposure	T opulation expe
Minimum frequency	0 Hz	Prevention of p
Maximum frequency	0 Hz	materials, and h
Function	bstatico.icnirp2009	
Reference document	ICNIRP Guidelines 2009 (S	tatic magnetic fields)

Restriction	Value
Occupational exposure, spatial peak in the head or trunk	2 T
Occupational exposure, specific applications in a controlled environment where appropriate work practices are implemented to control the effects induced by movement, spatial peak	8 T
Occupational exposure, spatial peak for exposure of limbs only	8 T
Population exposure, spatial peak in any part of the body	400 mT
Prevention of potential indirect side effects resulting from exposure of persons with implanted electronic medical devices and implants containing ferromagnetic materials, and hazards from flying metal objects: much lower maximum levels may be appropriate, up to	500 μΤ

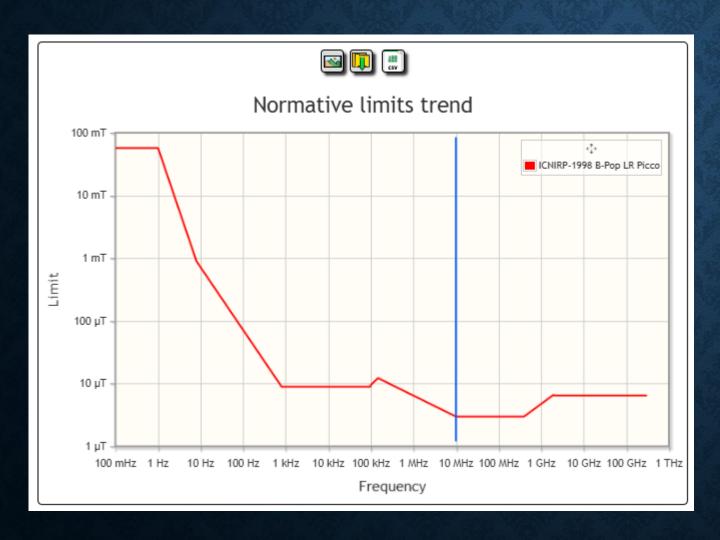


ICNIRP Guidelines 1998 - Magnet	ic induction - Limits for the general public - Peak reference levels Details Details
Short name	ICNIRP-1998 B-Pop LR Picco
Туре	Reference levels, action values (AV), action levels (AL)
Quantity	Magnetic flux density
Metric	Peak value
Subject	Population exposures
Effect	Undifferentiated
Level	Undifferentiated
Localization	Whole body exposure
Minimum frequency	0 Hz
Maximum frequency	300 GHz
Reference document	ICNIRP Guidelines 1998 (EMF up to 300 GHz)
Calculate limit at specific values	Frequency 300 GHz Calculate
	Limit

- Generic case: regulatory limit depends on the frequency
- User can calculate the limit at a specific frequency

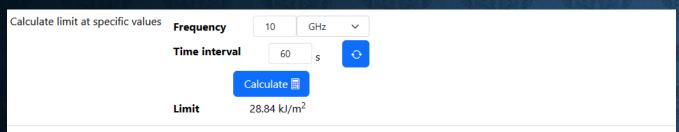
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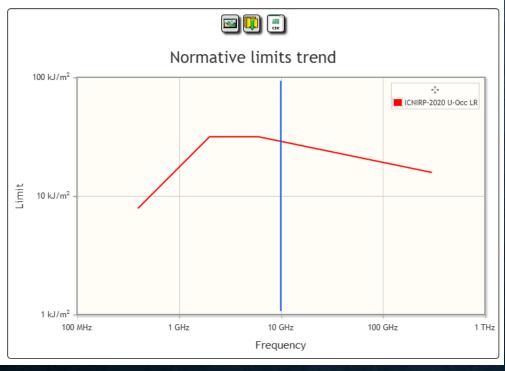




- Generic case: regulatory limit depends on the frequency
- User can calculate the limit at a specific frequency
- and plot limit trend vs. frequency

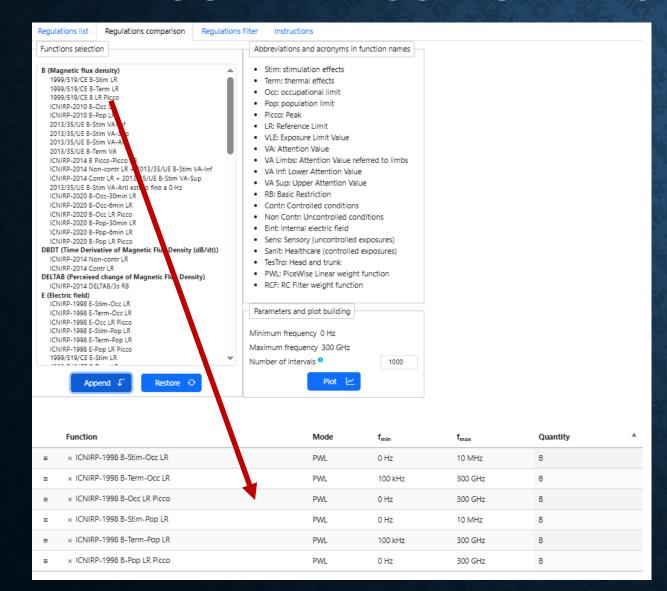






- In the 2020 ICNIRP guidelines, limits can depend:
 - on time
 - on frequency
 - on time AND frequency
- Calculation is performed at a specific time interval and frequency value
- Limit trend vs. frequency is displayed at the chosen time interval

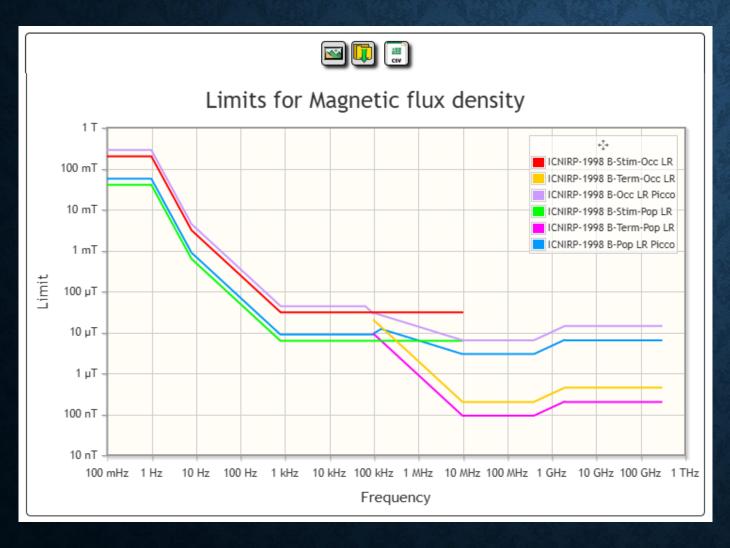




Comparison of limits:

- The user can select a set of limits to compare
- They are first displayed in a table, where user can set their order (as they will appear in plot)





Comparison of limits:

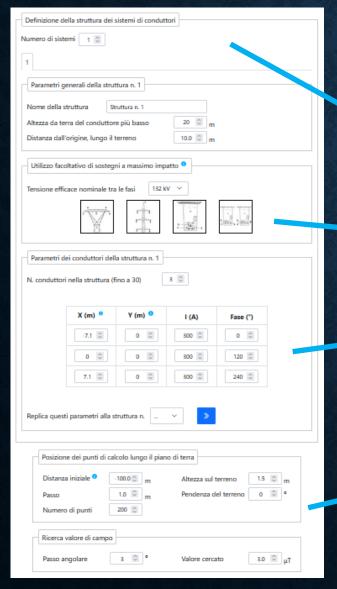
- The user can select a set of limits to compare
- They are first displayed in a table, where user can set their order (as they will appear in plot)
- and plot all of them (one physical quantity per graph)



2 sets of tools share a similar interface:

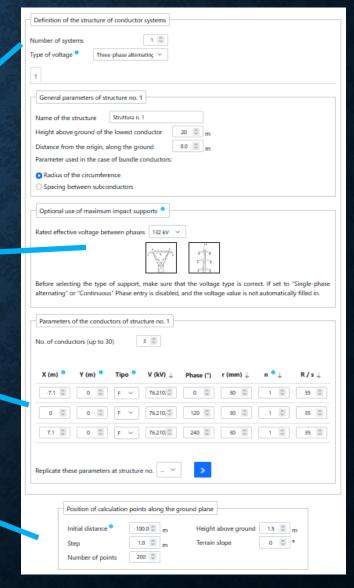
- Characterization of sources in the external environment
 - Calculation of the electric field / magnetic flux density generated by systems of indefinite rectilinear conductors
- Applications to support the reduction to compliance
 - Comparison of the electric field / magnetic flux density generated by systems of indefinite rectilinear conductors



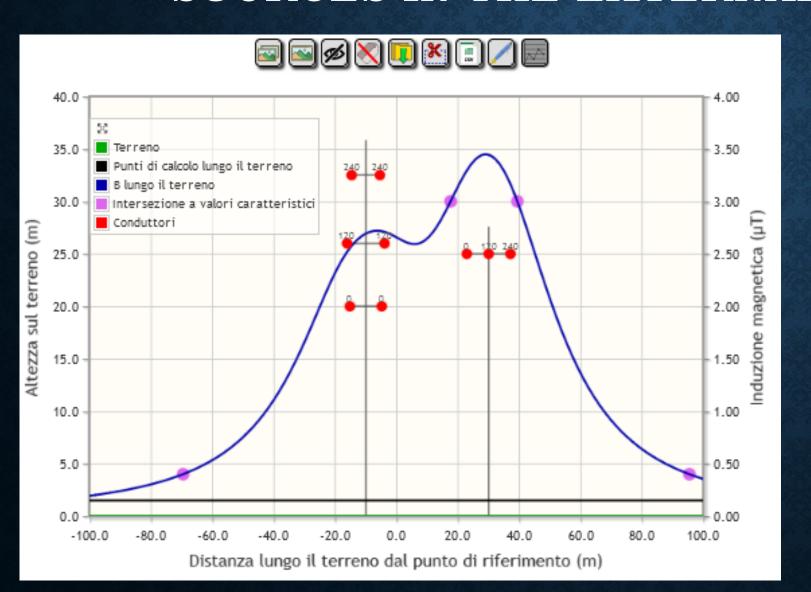


Calculating E or B

- User can define up to 10 power lines
- Eventually chose one from a database
- Insert power lines
 electric and geometric
 data
- Geometric calculation parameters

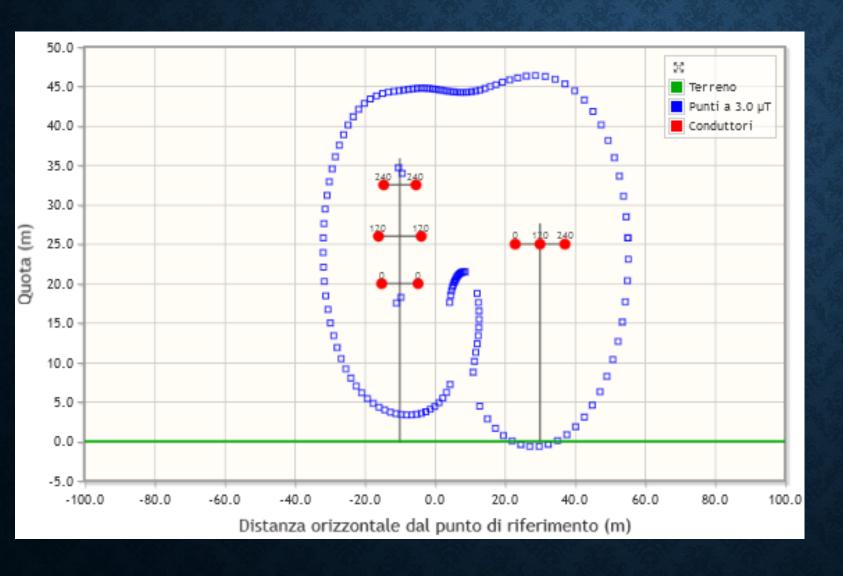






Magnetic flux density generated by systems of indefinite rectilinear conductors along a path parallel to the ground

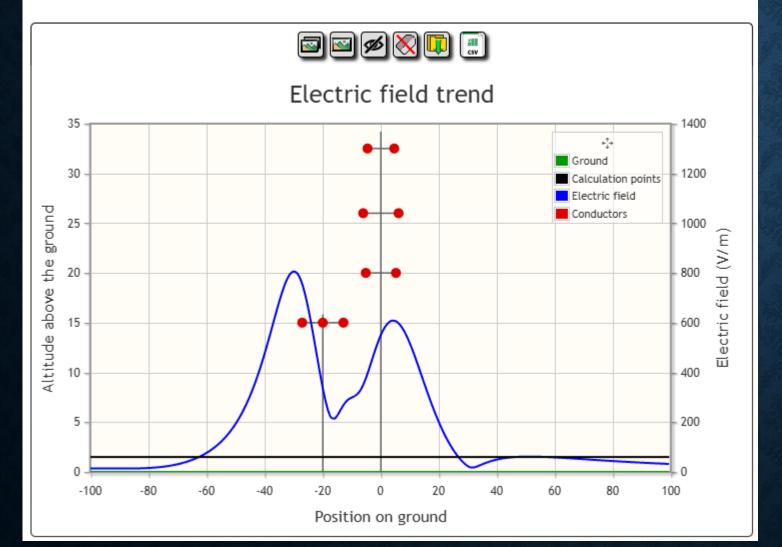




Position of points at a user-defined field value, around the wires

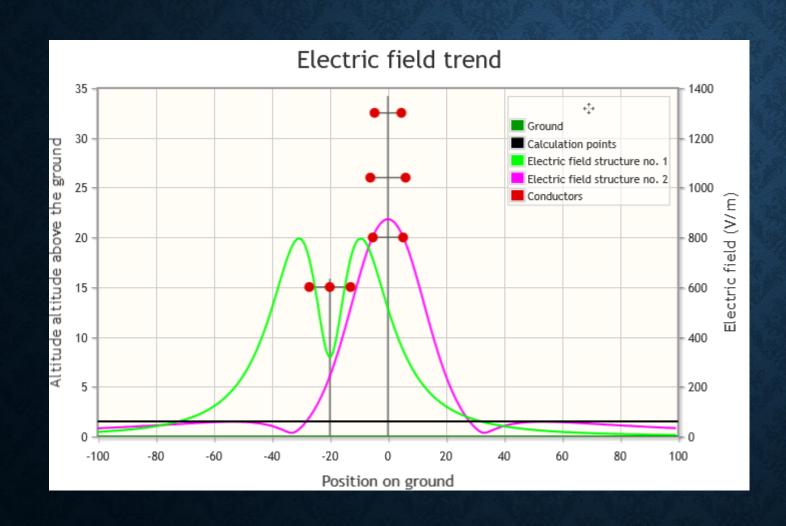


Peak value: 805.77 V/m at -30 m from origin.



Electric field generated by systems of indefinite rectilinear conductors





Comparison of the electric field generated by systems of indefinite rectilinear conductors



ANALYSIS OF COMPLEX SIGNALS

- General aspects
 - Interpolation of index measurements and calculation of the compliance distance with determination of the uncertainty
- Processing of data files from exposure measurements
 - Calculation of weighted peak indices for low and intermediate frequency magnetic field sources
 - Motion in a Static Magnetic Field Processing of Perceived Magnetic Field Measurements
 - Loading, recognition, and processing of measurement data files in the time or frequency domain



ANALYSIS OF COMPLEX SIGNALS

STANDARD METHOD

- 1. Compliance with the limit is given by this formula, in which an evaluation is made for each frequency component in relation to the limit referred to that frequency.
- 2. It is a very conservative approach, as it is not said that all the components have a maximum at the same instant (extremely improbable situation)

$$I_{MS} = \sum_{i=1}^{N} \frac{A_i}{L(f_i)} \leq 1$$

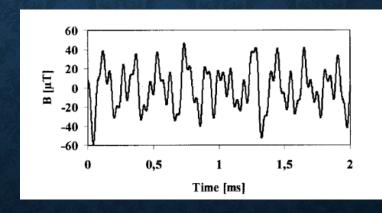


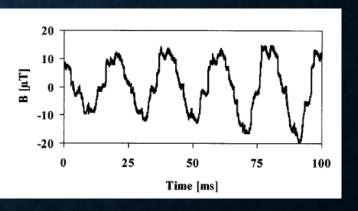
ANALYSIS OF COMPLEX SIGNALS

WEIGHTED PEAK METHOD (ICNIRP 2003-2010)

- Differences in phases between different components are considered
- 2. Avoid overestimating the effect of the signal in an overly conservative manner
- 3. The approach can be shown to be valid for complex coherent and incoherent signals (complex nonsinusoidal waveforms, with or without phase coherence)

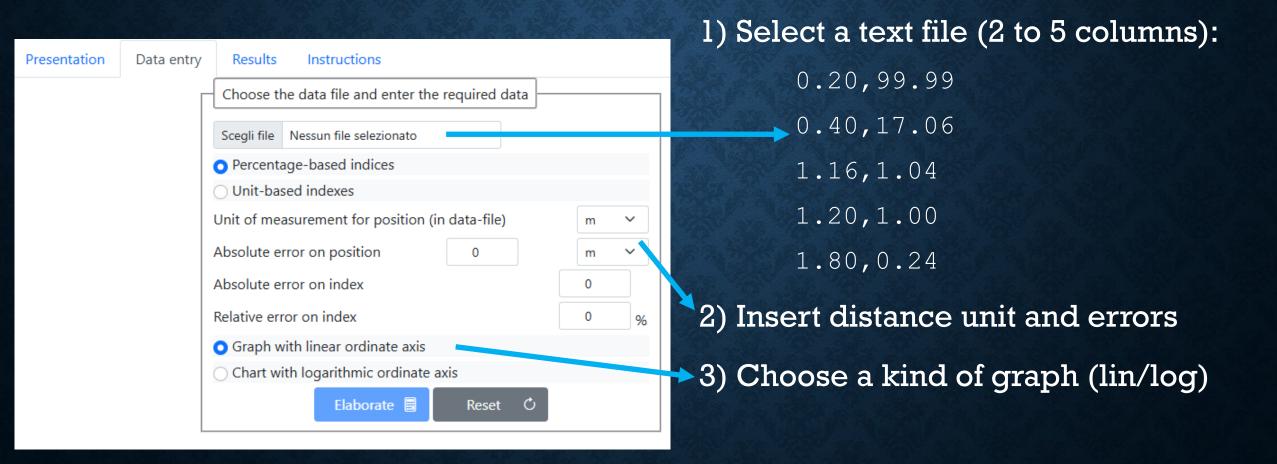
$$I_{WP} = Max \left| \sum_{i=1}^{N} \frac{A_i}{L(f_i)} \cos[2\pi f_i t + \vartheta_i + \varphi(f_i)] \right| \le 1$$





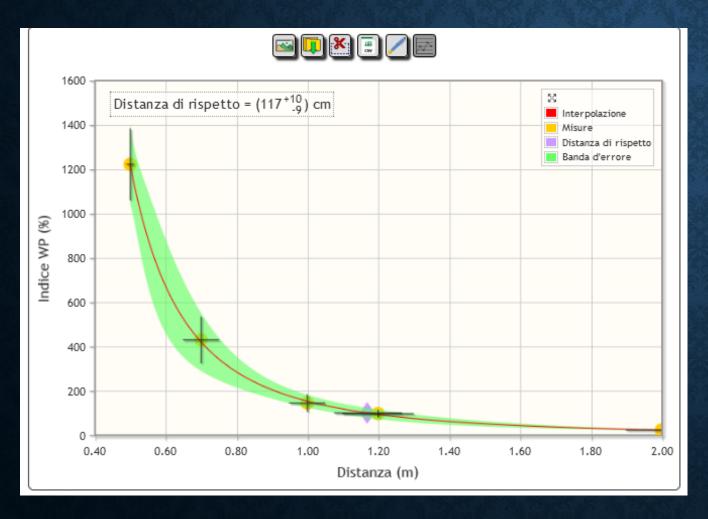


INTERPOLATION OF INDEX MEASUREMENTS AND CALCULATION OF THE DISTANCE OF RESPECT





INTERPOLATION OF INDEX MEASUREMENTS AND CALCULATION OF THE DISTANCE OF RESPECT



Interpolation with error bars and bands in a plot



3 applications:

- Motion in a static magnetic field: processing of perceived magnetic field measurements
- Calculation of weighted peak indices for low- and intermediatefrequency magnetic field sources
- Loading, recognition, and general processing of data files



Motion in a Static Magnetic Field and

Calculation of Weighted Peak Indices:

- First procedures developed
- They are structured on the characteristics of specific measuring instruments, implementing specific scanning algorithms for the known output file format.



Motion in a Static Magnetic Field - Processing of Perceived Magnetic Field Measurements

- Assessment of occupational exposure due to an operator's movement in any non-homogeneous magnetic field
- Narda-Metrolab THM-1176 probe, attached to a specific point on the operator's body
- The probe is connected via USB cable to a PC running the probe management software



Motion in a Static Magnetic Field - Processing of Perceived Magnetic Field Measurements

Narda-Metrolab THM-1176 probe







Motion in a Static Magnetic Field - Processing of Perceived Magnetic Field Measurements

- The subject is asked to perform movements typical of the various activities performed in relation to the task being studied, in areas where an intense static magnetic field is present
- During these movements, the instantaneous values of the magnetic induction vector detected by the probe are stored in a file on the personal computer
- The web tool allows processing of the data files



Motion in a Static Magnetic Field - Processing of Perceived Magnetic Field Measurements

This instrument allows processing of magnetic field measurements that vary very slowly over time to derive the radiation protection parameters required by the ICNIRP-2014 "Guidelines for limiting exposure to electric fields induced by movement of the human body in a static magnetic field and by time-varying magnetic fields below 1 Hz":

- the maximum ΔB variation in any 3-second interval
- the weighted peak index for stimulation effects.



Calculation of weighted peak indices for low and intermediate frequency magnetic field sources

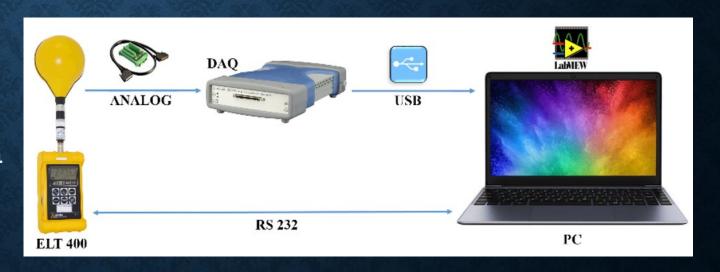
- A methodology for acquiring gradient magnetic field waveforms in the time domain has been developed.
- These waveforms are also essential for determining the weighted peak indices.



Calculation of weighted peak indices for low and intermediate frequency magnetic field sources

Measurement chain:

- Narda ELT-400 meter with 100 cm² probe
- Agilent U2351A data acquisition system (connected to the meter's analog output)
- PC connected to both the data acquisition system via a USB connection and the meter via a standard RS232 connection
- On the PC: data acquisition and chain management program, developed by ENEA in a LabVIEW environment.





Calculation of weighted peak indices for low and intermediate frequency magnetic field sources

- This web tool allows you to process the data files produced by that instrument chain, which therefore relate to low-frequency magnetic flux density measurements (not limited to gradient fields in MRI).
- The radiation protection parameters required by law are derived, including the weighted peak indices for stimulation effects referred to any regulatory limit (not just those for which the index is provided directly from the meter display).



This approach used in the 2 tools has been expanded in order to accept files of the most generic type possible, potentially produced by <u>any</u> measurement chain, as long as they are in an open format (text file or spreadsheet). 2 possibilities:

- Measurement chain already known to the system (stored in the database)
- Measurement chain not present in the database. The user provides the description of the data format.



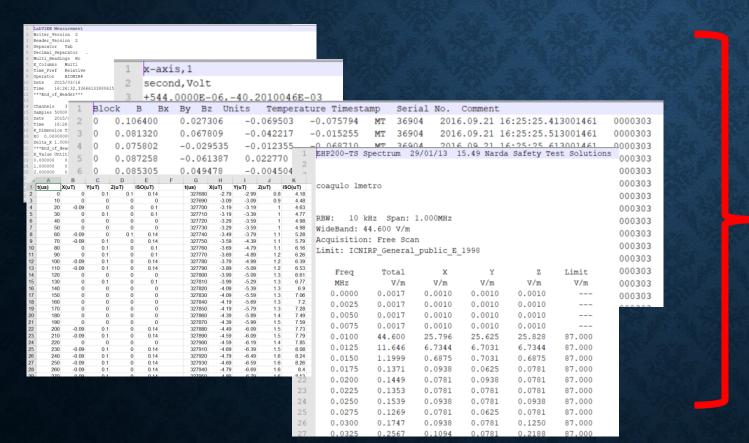
Loading, recognition, and processing of measurement data files in the time or frequency domain

Application structured in 3 sections (time domain, frequency domain, generic data), providing:

- Procedures developed for specific chains (divided into time and frequency domains)
- Generalized acquisition system for data files obtained from chains stored in DB
- Generalized acquisition for data files obtained from chains not stored in DB: the user must provide information about the structure of the data file



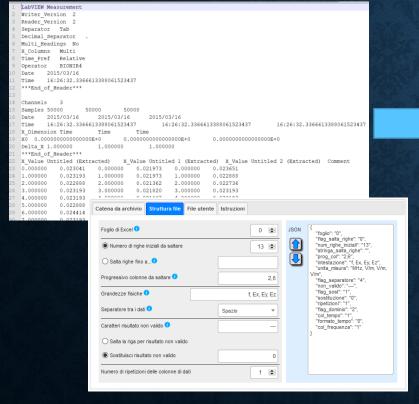
Creating homogeneous format files



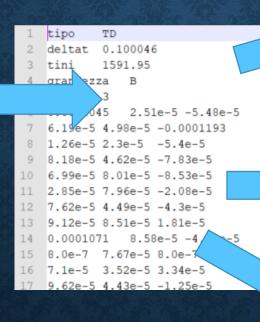
```
tipo
        0.100046
tini
        1591.95
grandezza
colonne 3
0.0001045
                   grandezza
                   colonne 3
                            0.0017
                            0.0017
                   20000
                            0.1449
                   22500
                            0.1353
                   25000
                            0.1539
                   27500
                   30000
```

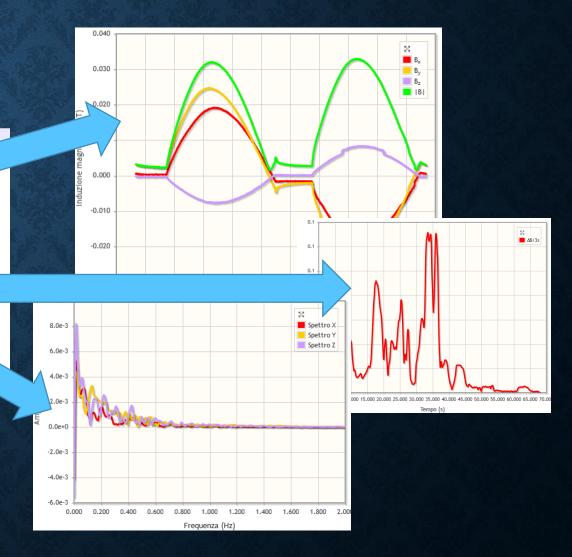


Data file



Standard file



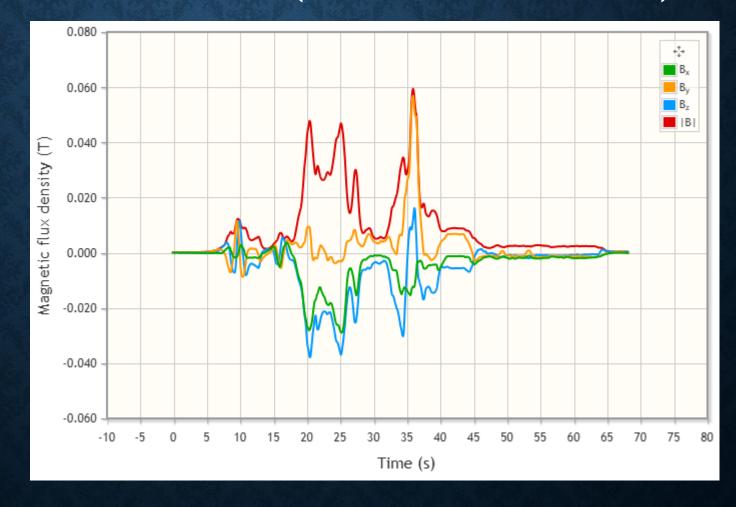


Information on file structure



Data output: components and module of H/B/E fields (condensed or all-data modes)

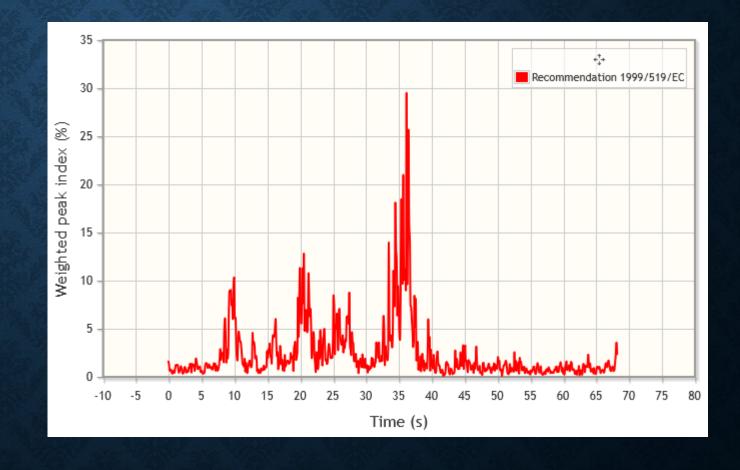
Data summary				
User file	magnet_2010.txt			
Quantity	B (T)			
Number of samples	683			
Sampling period	100.1 ms			
Overall duration	68.34 s			
Maximum modulus value	59.40 mT @ 36.02 s			
RMS value	15.67 mT			





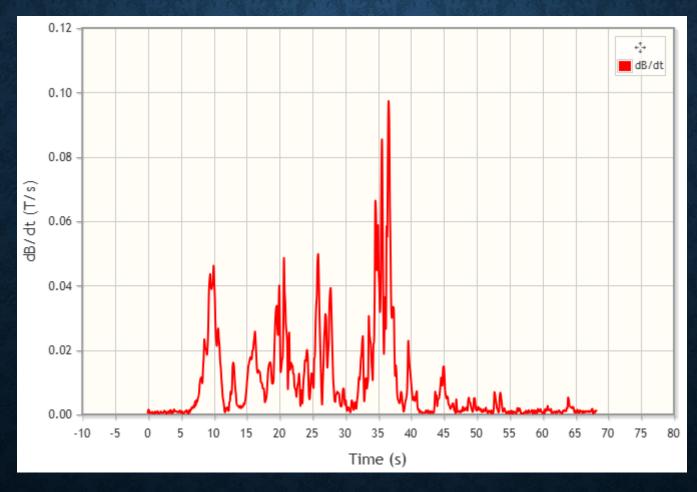
Data output: wheighted peak indices, according to different regulations

Weighted peak indices				
Standard file format: <u>wp202509051335381757072138338.txt</u>				
Recommendation 1999/519/EC	29.5%			
ICNIRP 1998 Workers	5.9%			
ICNIRP 2010 Workers	7.7%			
D.Lgs. 81/2008 Lower AV	7.7%			
D.Lgs. 81/2008 Upper AV	3.7%			
Legislative Decree 81/2008 AV in limbs	1.2%			



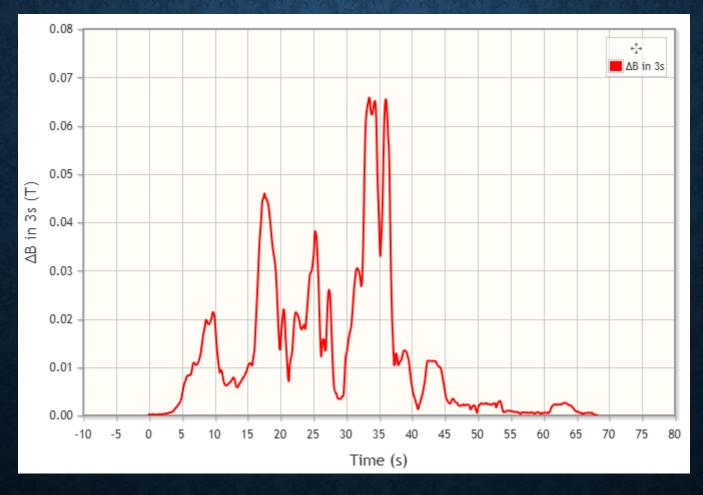


Data output: trend of dB/dt



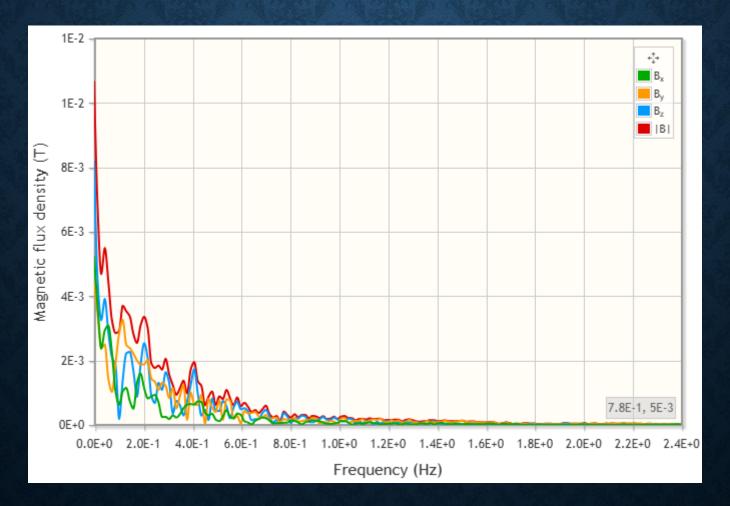


Data output: Max $\Delta B/3s$ and its trend over time



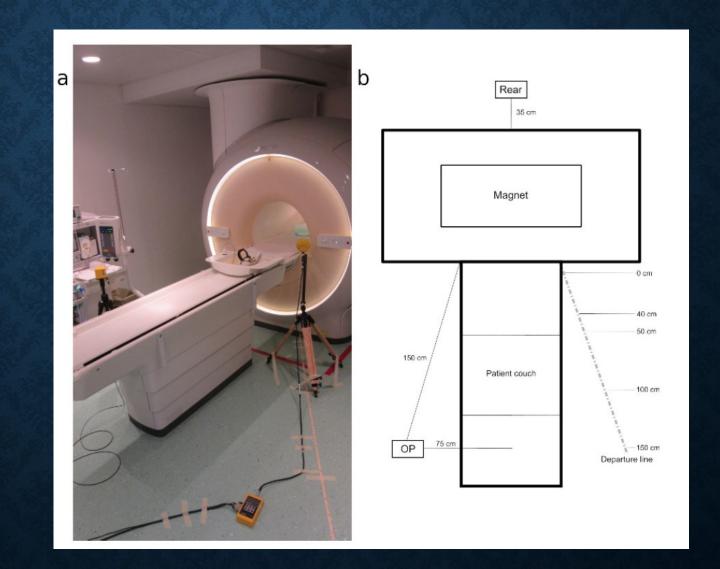


Data output: spectrum in continuous/discrete format





Tests carried out on different tomographs (1 and 1.5 T)





Different instrumental chains:

- Narda ELT-400 probe, data acquired via Agilent ADC
- Narda ELT-400, stand alone setup
- Narda EHP-50F





Different instrumental chains:

- Narda ELT-400 probe, data acquired via Agilent ADC: provides raw data (analog output), skilled personnel required for data analysis
- Narda EHP-50F: Provides indexes, but no further analysis is possible



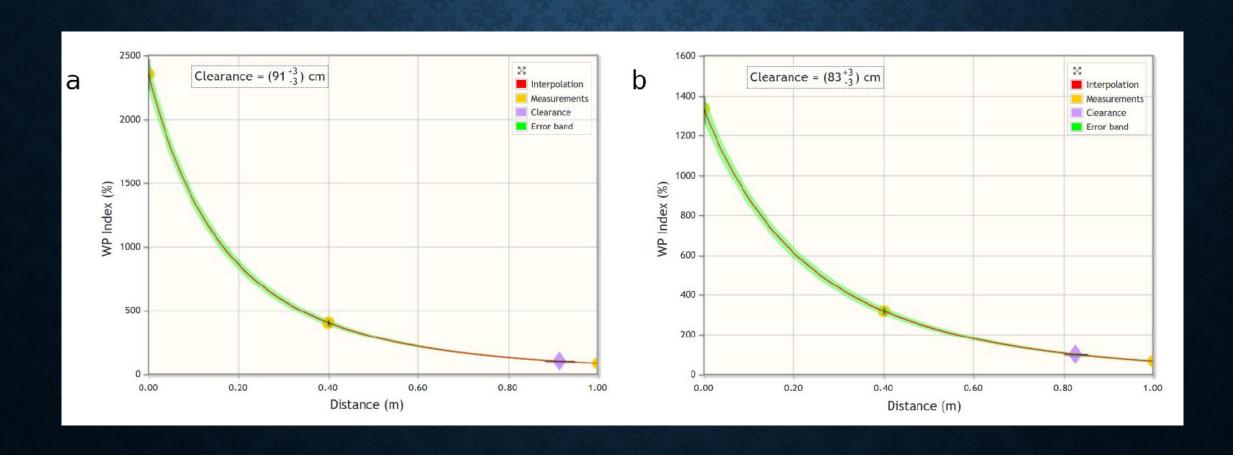


Iwp are calculated at different distances from the gantry

Sequence	Distance (cm)	Height (cm)	RLs 1999/519/EC	Low ALs 2013/35/EU	High ALs 2013/35/EU
B1	0	100	1389%	45.0%	45.6%
	OP		22.5%	0.70%	0.60%
B2	0		2356%	76.0%	72.5%
	40	100	401%	13.0%	12.0%
	100		83%	2.50%	2.10%
	OP	-	51%	1.57%	1.25%
	0	160	1332%	40.1%	40.8%
	40		317%	9.70%	9.17%
	100	-	66%	2.00%	1.65%

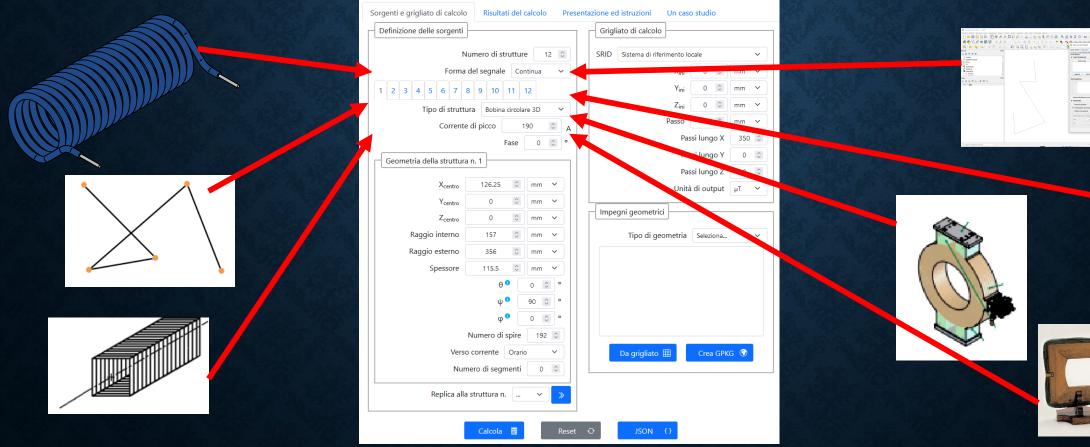


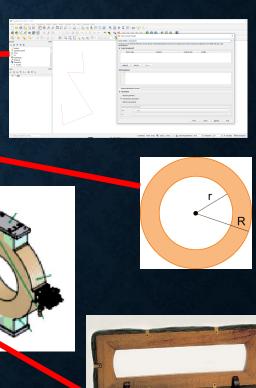
Interpolation of indices is performed to get a compliance area





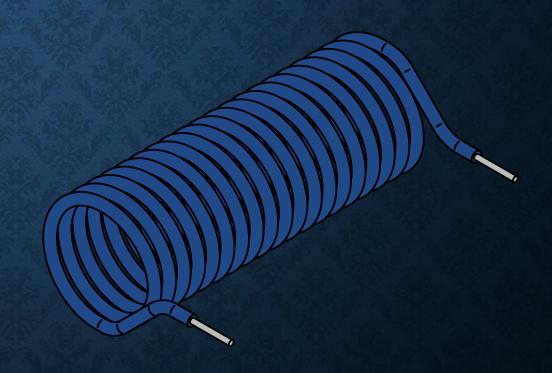
An application calculates the magnetic flux density generated by a system of various kinds of conductors, whose geometries can be defined as combination of several basic models.





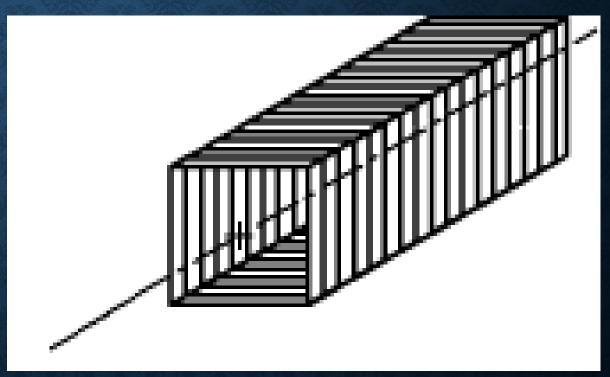


- Circular section solenoid
- Rectangular section solenoid
- Corona coil
- 3D circular coil
- 3D rectangular coil
- Broken line
- Catenary
- Geometry imported from GIS files



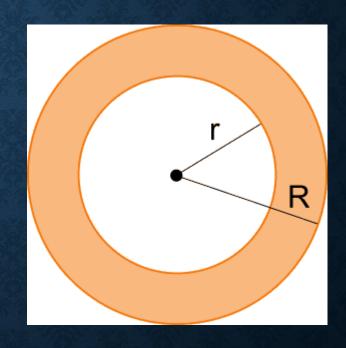


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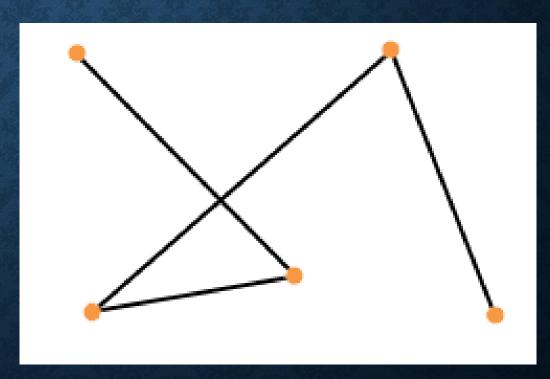


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- Catenary
- Geometry imported from GIS files



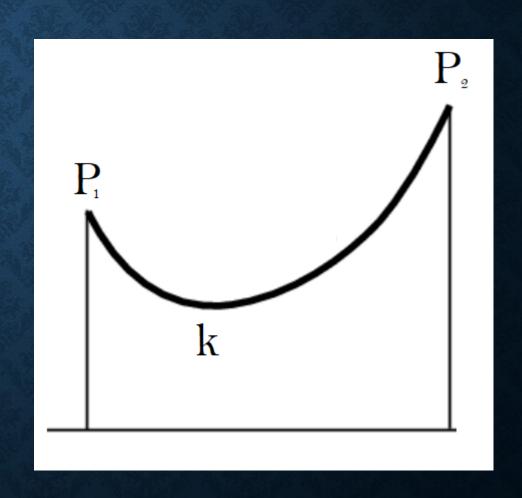


- Circular section solenoid
- Rectangular section solenoid
- Corona coil
- 3D circular coil
- 3D rectangular coil
- Broken line
- Catenary
- Geometry imported from GIS files



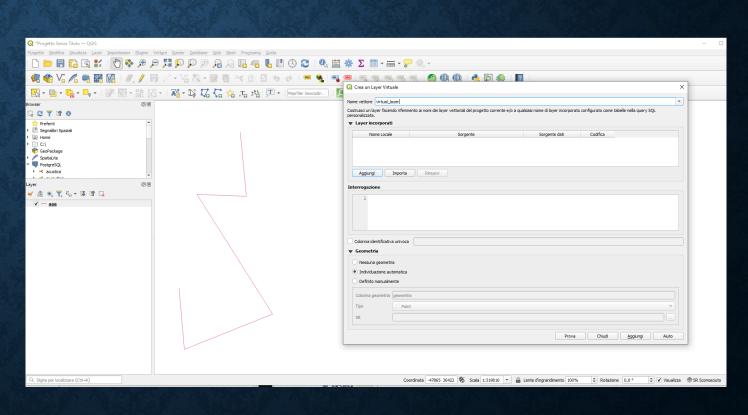


- Circular section solenoid
- Rectangular section solenoid
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- 3D circular coil
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- Circular section solenoid
- Rectangular section solenoid
- Corona coil
- 3D circular coil
- 3D rectangular coil
- Broken line
- Catenary
- Geometry imported from GIS files





In the various types of sources, the simplest constituent element can be:

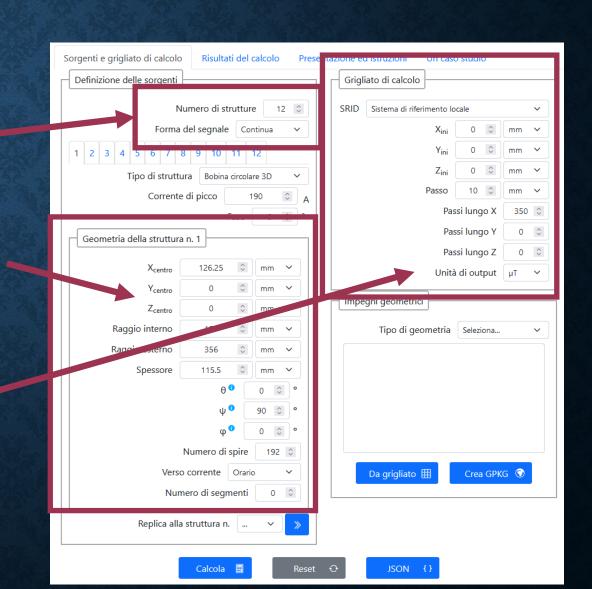
- a segment (as in the case of the catenary, which is approximated by a broken line)
- a circular loop

The contribution of the field at each point of the calculation grid is determined for each elementary source (segment or circular loop) and the results are then added.



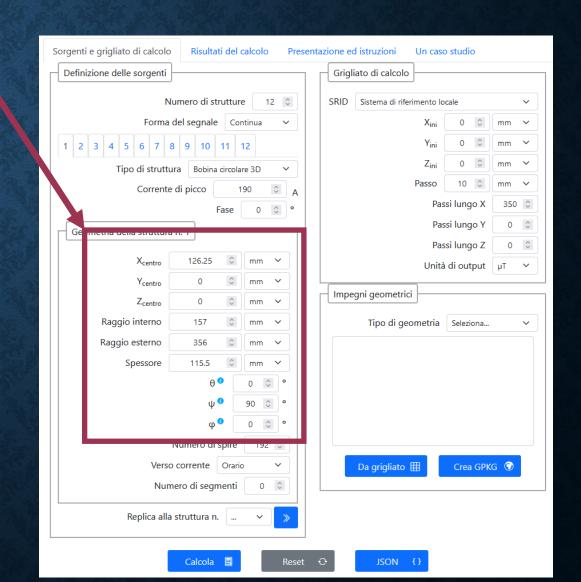
The user can:

- specify up to 12 configurations of conductors of these types
- define their geometric and electrical characteristics
- calculate the value of magnetic induction in a regular grid



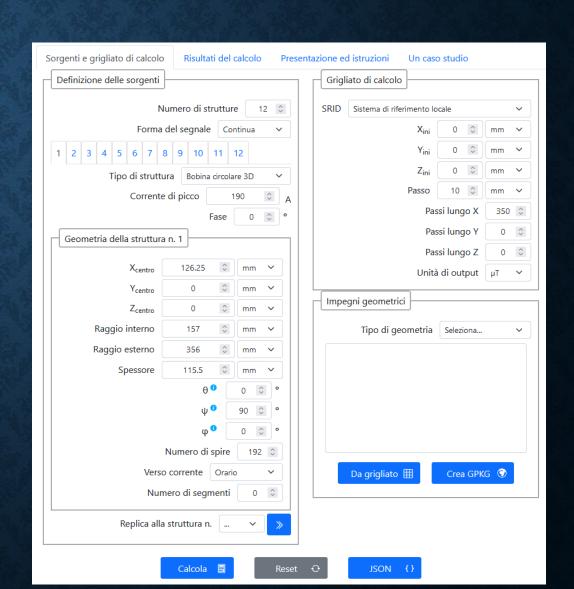


- Geometries can be positioned and oriented appropriately in space
- Any set of conductors that can be represented as a combination of simple configurations can be described.





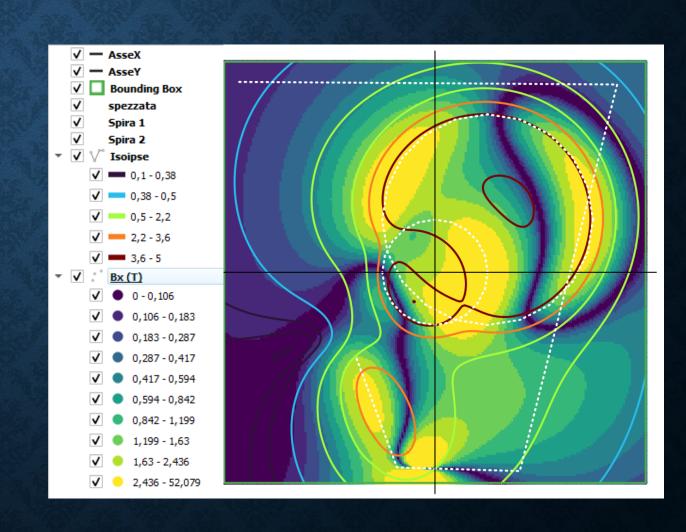
- The calculation is performed in free space
- The presence of ferromagnetic elements inside the coils is not considered
- Nor other objects in the surrounding space





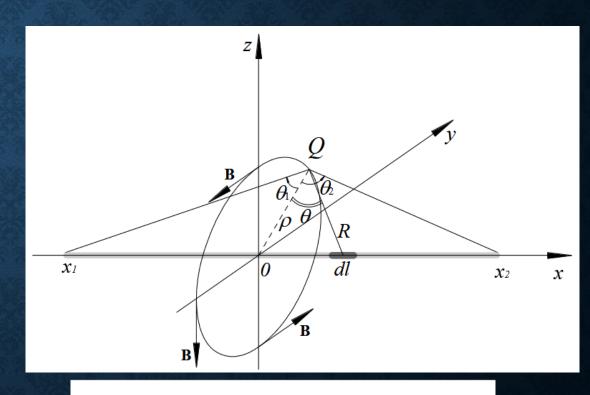
Example of expected output:

- 3 simple sources (one broken line, 2 circular loops)
- Field map in QGIS
- Isohypses
- Overlap with sources and bounding boxes (of the calculation grid)





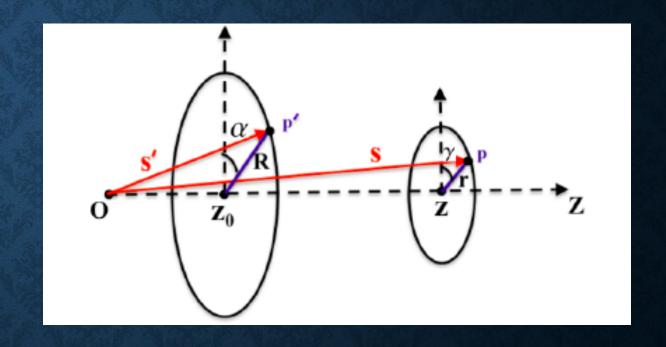
The solution to the field calculation of a segment carrying current is quite simple.



$$\mathbf{B} = \frac{\mu_0 I}{4\pi\rho} \left(\sin\theta_2 - \sin\theta_1\right) \hat{\varepsilon}$$



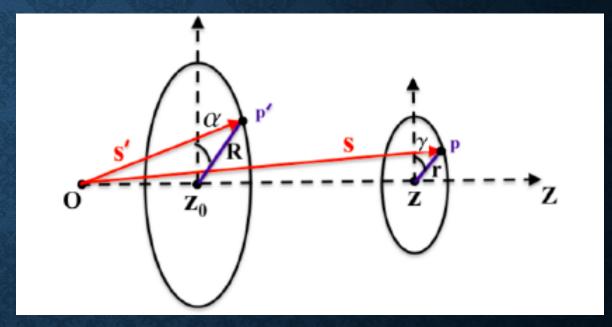
- The solution in all space in the case of a circular loop requires more complex mathematical considerations
- It starts from the determination of the vector potential.



Magnetic flux is a zero-divergence field, it can be expressed as a curl of a potential field:

$$\vec{B} = \vec{\nabla} \times \vec{A}$$

and by choosing the Coulomb gauge we get the solution:



$$\vec{A} = \frac{\mu_0 I}{4\pi} \oint_C \frac{\vec{dl}}{s}$$



The longitudinal and radial components for the magnetic flux density are obtained:

$$B_z = \frac{\mu_0 I}{2\pi\sqrt{z^2 + (R+r)^2}} \left(\frac{R^2 - z^2 - r^2}{z^2 + (r-R)^2} E(k) + K(k) \right)$$

$$B_r = \frac{\mu_0 z I}{2\pi r \sqrt{z^2 + (R+r)^2}} \left(\frac{R^2 + z^2 + r^2}{z^2 + (R-r)^2} E(k) - K(k) \right)$$

E, K: complete elliptic integrals of I and II species

$$k = 2\sqrt{\frac{rR}{z^2 + (R+r)^2}}$$

$$E_1(k) = \int_0^{2\pi} \frac{d\theta}{\sqrt{1 - k^2 (\sin \theta)^2}}$$

$$E_2(k) = \int_0^{2\pi} \sqrt{1 - k^2 (\sin \theta)^2} d\theta$$



An alternative procedure, proposed by INFN, leads to:

$$B_r = \frac{\mu_0 I M_z}{2R} \left[\frac{\xi}{2\eta(1+\xi)} \right]^{\frac{3}{2}} \left[{}_2F_1 \left(\frac{3}{2}, \frac{3}{2}; 2; \frac{2\xi}{1+\xi} \right) - {}_2F_1 \left(\frac{1}{2}, \frac{3}{2}; 1; \frac{2\xi}{1+\xi} \right) \right]$$

$$B_{z} = \frac{\mu_{0}I}{2R} \left[\frac{\xi}{2\eta(1+\xi)} \right]^{\frac{3}{2}} \left[(\eta+1)_{2}F_{1}\left(\frac{1}{2},\frac{3}{2};1;\frac{2\xi}{1+\xi}\right) - \eta_{2}F_{1}\left(\frac{3}{2},\frac{3}{2};2;\frac{2\xi}{1+\xi}\right) \right]$$

$$\xi = \frac{2rR}{r^2 + R^2 + (z - z_0)^2}$$

$$\eta = \frac{r}{R}$$

$$M_z = \frac{z}{R}$$

The mathematical equivalence of the two methods is demonstrated using the relations:

$$E\left(\frac{2\xi}{\xi+1}\right) = \frac{\pi}{2} \frac{1-\xi}{1+\xi} \, _2F_1\left(\frac{1}{2}, \frac{3}{2}; 1; \frac{2\xi}{1+\xi}\right)$$

$${}_{2}F_{1}\left(\frac{3}{2},\frac{3}{2};2;\frac{2\xi}{1+\xi}\right) = \frac{4E\left(\frac{2\xi}{\xi+1}\right) + \left(\frac{\xi-1}{\xi+1}\right)K\left(\frac{2\xi}{\xi+1}\right)}{\frac{2\pi\xi(1-\xi)}{(\xi+1)^{2}}}$$



VALIDATION OF THE PROCEDURE

An internal validation of the software results was performed by comparing:

- the exact formulation that uses elliptic integrals
- the exact formulation that uses the hypergeometric function
- the approximate calculation in which the loop is approximated with a broken line, progressively increasing the number of segments constituting the single loop (tests were performed by approximating the loop with 20, 200, and 2000 segments)



VALIDATION OF THE PROCEDURE

Validation result:

- The result obtained in the first 2 cases is coincident up to the 13th digit, the 2 formulations are equivalent, and the discrepancies are due to the implicit approximations in the libraries used. In particular, the language used to perform the calculations is Python 3.9 and the SciPy.special library is used to calculate elliptic integrals and hypergeometric functions.
- The comparison of these results with those obtained from the approximation with a broken line showed a progressive convergence in the number of identical digits as the number of segments with which the loop is approximated increases.
- Warning: very different calculation times (10x with a loop approximated by 20 segments)



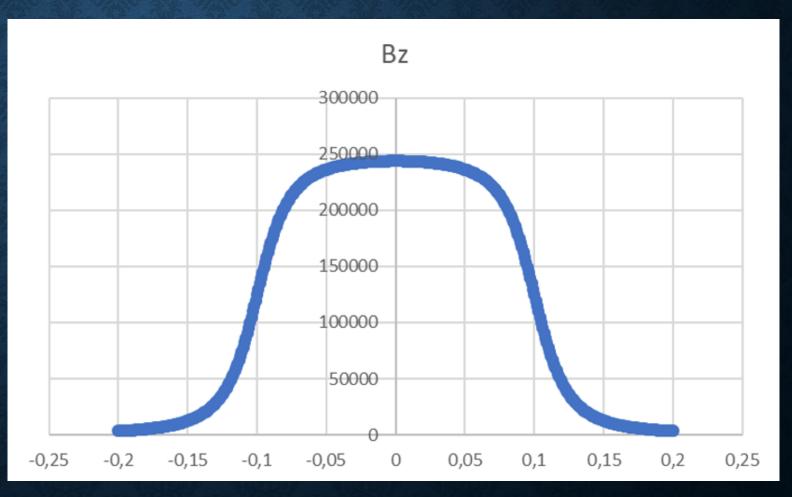
VALIDATION OF THE PROCEDURE

Finally, the expected result at the center of a solenoid:

- 200 coils
- radius: 25 mm
- distance between coils: 1 mm
- current intensity: 200 A

coincides with that expected from the theory for the infinite solenoid:

$$B = \frac{\mu_0 NI}{l}$$





THE RESULTS OF THE CALCULATION

At the end of the calculation:

- some summary values of interest are displayed (calculation time, minimum and maximum values of the induction module)
- it is possible to download the text file containing the results:

Marie Contract of the Contract					
Y	Z	B Bx	Ву	Bz	
0.0	0.0	628.3185307179	0.0	0.0	628.3185307179
1.0	0.0	0.317730752302	0.0	0.0	0.317730752302
2.0	0.0	0.039380643144	0.0	0.0	0.039380643144
3.0	0.0	0.011650089610	0.0	0.0	0.011650089610
4.0	0.0	0.004912192226	0.0	0.0	0.004912192226
5.0	0.0	0.002514405568	0.0	0.0	0.002514405568
6.0	0.0	0.001454895688	0.0	0.0	0.001454895688
7.0	0.0	0.000916126557	0.0	0.0	0.000916126557
8.0	0.0	0.000613700191	0.0	0.0	0.000613700191
9.0	0.0	0.000431005356	0.0	0.0	0.000431005356
98.0	0.0	0.000000114455	0.0	0.0	0.000000114455
99.0	0.0	0.000000112751	0.0	0.0	0.000000112751
100.0	0.0	0.000000111072	0.0	0.0	0.000000111072
	0.0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0	0.0 0.0 1.0 0.0 2.0 0.0 3.0 0.0 4.0 0.0 5.0 0.0 6.0 0.0 7.0 0.0 8.0 0.0 9.0 0.0	0.0 0.0 628.3185307179 1.0 0.0 0.317730752302 2.0 0.0 0.039380643144 3.0 0.0 0.011650089610 4.0 0.0 0.004912192226 5.0 0.0 0.002514405568 6.0 0.0 0.001454895688 7.0 0.0 0.000916126557 8.0 0.0 0.000613700191 9.0 0.0 0.000003114455 99.0 0.0 0.0000000112751	0.0 0.0 628.3185307179 0.0 1.0 0.0 0.317730752302 0.0 2.0 0.0 0.039380643144 0.0 3.0 0.0 0.011650089610 0.0 4.0 0.0 0.004912192226 0.0 5.0 0.0 0.002514405568 0.0 6.0 0.0 0.001454895688 0.0 7.0 0.0 0.000916126557 0.0 8.0 0.0 0.000613700191 0.0 9.0 0.0 0.000431005356 0.0 99.0 0.0 0.000000114455 0.0 99.0 0.0 0.0000000112751 0.0	0.0 0.0 628.3185307179 0.0 0.0 1.0 0.0 0.317730752302 0.0 0.0 2.0 0.0 0.039380643144 0.0 0.0 3.0 0.0 0.011650089610 0.0 0.0 4.0 0.0 0.004912192226 0.0 0.0 5.0 0.0 0.002514405568 0.0 0.0 6.0 0.0 0.001454895688 0.0 0.0 7.0 0.0 0.000916126557 0.0 0.0 8.0 0.0 0.000613700191 0.0 0.0 99.0 0.0 0.000000114455 0.0 0.0 99.0 0.0 0.0000000112751 0.0 0.0

Ready to be imported in Excel, QGIS...



THE RESULTS OF THE CALCULATION

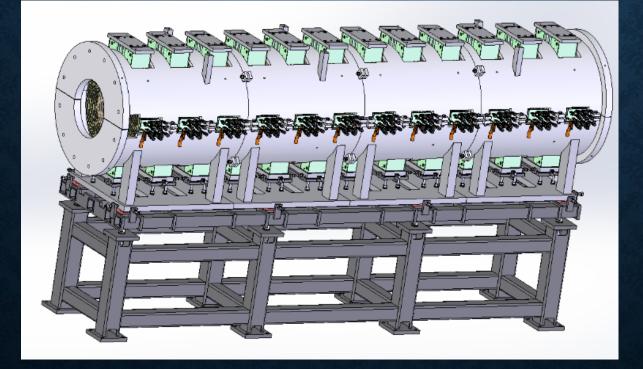
At the end of the calculation:

- ...
- it is possible to download a zip file containing the source geometries in GeoPackage format
- it is possible to set 2 values (for 2 Cartesian axes) among those for which the calculation was performed in the grid and display the trend of the field (modulus and components) along the third coordinate in the graph.



In the accelerator field, there are several relevant applications of focusing systems for charged particle beams using magnetic

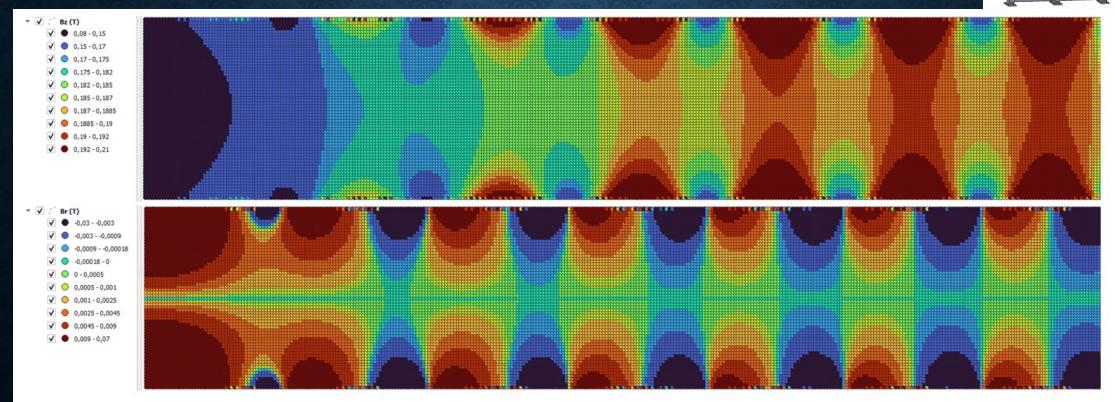
lenses.





Maps with the axial (above) and radial (below) field components.

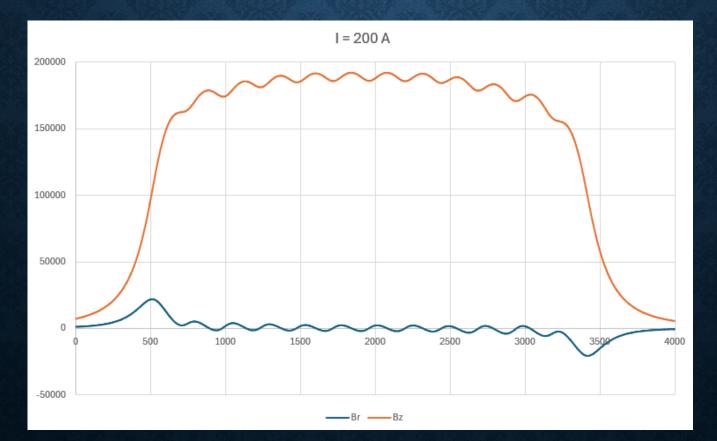






Trend of the radial (in blue) and axial (in orange) components of the induction along a trajectory parallel to the central axis of the structure.

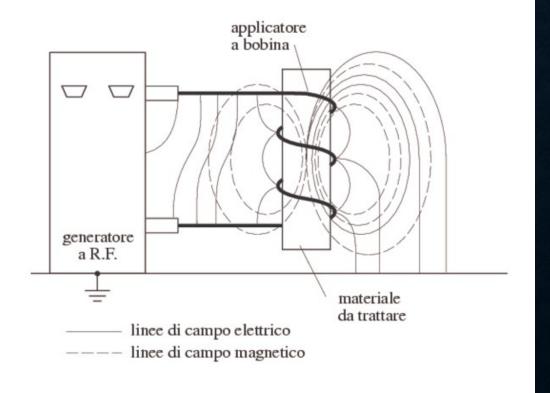






In the field of radiation protection, a case study is that of exposure to the magnetic field generated by an induction furnace used in the goldsmith industry.

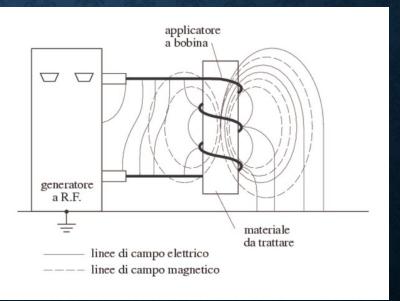






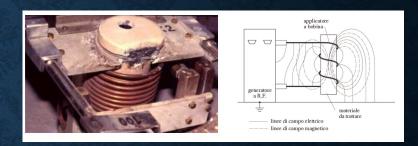
- It is a solenoid wrapped around a cylindrical crucible, connected to a radio frequency generator.
- It uses strong magnetic fields to induce eddy currents in the metals to be worked, heating them until they melt.
- Typical working frequencies range from a few kHz to a few tens of kHz.

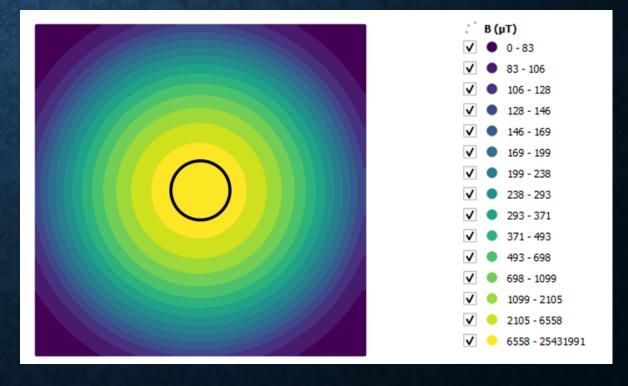






- The results of the calculation are reported, displayed in QGIS, and superimposed on the source geometry (in the horizontal plane), automatically exported by the calculation program in geoPackage format.
- The results are consistent with the simulations performed when the device was analyzed.







2 specific tools dedicated to AIMD available on WebNIR platform:

- Estimation of the voltage induced at the input of a pacemaker
- Operational indications for risk assessment in workers with AIMD

Documents about Source recognition and characterization:

- RFID
- UMTS and LTE
- Wi-Fi and Bluetooth



The tool allows to calculate the voltage induced at the input terminals of a pacemaker, according to its exposure conditions (the values of electric field intensity and/or magnetic field), through the implementation of the formulas reported in the appendix of the standard CEI EN 50527-2-1 ed. 2 (2016).



Estimation of the induced voltage (green symbol in the graph) across a pacemaker as a function of the electric and magnetic field – worst case conditions on a loop of area = 225 cm².

 $\mathbf{V}_{pp}^{\quad ind,max}$: maximum induced voltage in open circuit, expressed as a peak-to-peak value (V)

 $\mathbf{E}(t)$: instantaneous value of the measured electric field (V/m)

 $\mathbf{B}(t)$: instantaneous value of the measured magnetic field (A/m)

Frequency range	$\mathbf{V}_{pp}^{ind,max}$ ()		Paragraph Standard 50527-2-1	
[16.6 Hz; 60 Hz]	Unipolar	$\max(3,6\cdot10^{-7}\cdot \mathbf{H}(t) +4,4\cdot10^{-9}\cdot \mathbf{E}(t))\cdot f$	5254	
	Bipolar	$\max(1, 8 \cdot 10^{-8} \cdot \mathbf{H}(t) + 2, 3 \cdot 10^{-10} \cdot \mathbf{E}(t)) \cdot f$	E.3.5.1	
[60 Hz; 150 kHz] ⁰	Unipolar	$3,6\cdot 10^{-7}\cdot \mathbf{H}_p\cdot f$	E.3.3	
	Bipolar	$1,8\cdot 10^{-8}\cdot \mathbf{H}_p\cdot f$		
[150 kHz; 5 MHz]		$3,6\cdot 10^{-10}\cdot \sqrt{10^{6}\cdot \mathbf{H}_{p}^{2}+ \mathbf{E}_{p}^{2}}\cdot f$	E.3.6	
[5 MHz; 30 MHz]		$\max \begin{cases} 6 & 55 \cdot 10^{-10} \cdot \mathbf{H}_{p} \cdot f^{1,4} \\ 3 & 6 \cdot 10^{-10} \cdot \sqrt{10^{6} \cdot \mathbf{H}_{p}^{2} + \mathbf{E}_{p}^{2}} \cdot f \\ 3 & 17 \cdot 10^{-16} \cdot \mathbf{E}_{p} \cdot f^{1,9} \end{cases}$	E.3.7	
[30 MHz; 200 MHz]	$5.1 \cdot 10^{-2} \cdot \max \begin{Bmatrix} 377 \cdot \mathbf{H}_p \\ \mathbf{E}_p \end{Bmatrix}$			
[200 MHz; 400 MHz]		$4.1 \cdot 10^{23} \cdot \max \begin{Bmatrix} 377 \cdot \mathbf{H}_p \\ \mathbf{E}_p \end{Bmatrix} \cdot f^{-3}$	E.3.8	
[400 MHz; 450 MHz]		$6,37 \cdot 10^{-3} \cdot \max \begin{Bmatrix} 377 \cdot \mathbf{H}_p \\ \mathbf{E}_p \end{Bmatrix}$		



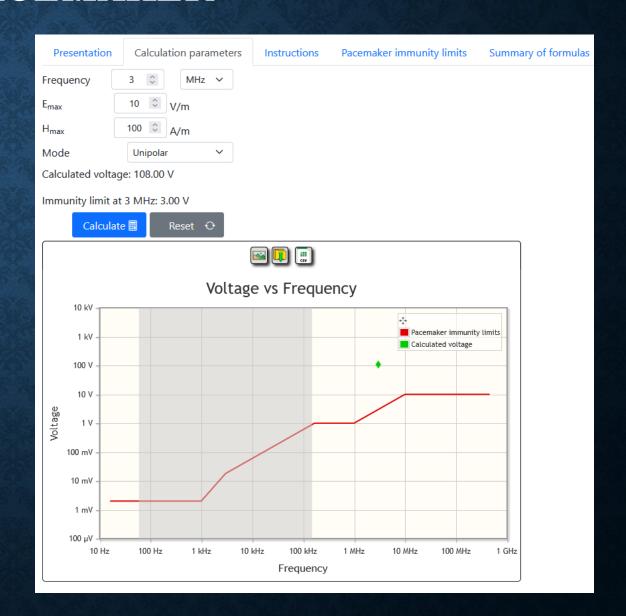
The induced voltage value obtained can be compared with the immunity levels that pacemakers must satisfy, at various frequencies (16.6 Hz - 60 Hz, and 150 kHz - 450 MHz), to verify their compatibility under actual exposure conditions.

In the range between 60 Hz and 150 kHz there are no validated studies that allow the electric field to be correlated with the induced voltage on the pacemaker, therefore the instrument does not support this frequency range. The calculation is performed for a purely magnetic field.



The calculation is performed by entering the frequency of interest and the maximum peak values of the electric and magnetic fields measured.

The induced voltage value obtained is compared with the immunity levels that pacemakers must satisfy, at the various frequencies, in the conducted immunity tests provided for in the technical standard EN 45502-2-1:2003 (table in next slide).





Immunity limits of pacemakers (red line in the graph) for conducted disturbances in the frequency range [16 Hz; 450 MHz] according to the tests indicated in *Standard 45502-2-1: Active implantable medical devices*.

Frequency range	Test signal amplitude (peak-to-peak)	Paragraph Standard 45502-2-1	
[16.6 Hz; 1 kHz]	2mV		
[1 kHz; 3 kHz]	$2mV \cdot \left(\frac{f}{1kHz}\right)^2$	27.5.1	
[3 kHz; 167 kHz]	$6mV \cdot \left(\frac{f}{1kHz}\right)$		
[167 kHz; 1 MHz]	1V		
[1 MHz; 10 MHz]	$1V \cdot \left(\frac{f}{1MHz}\right)$	27.5.2	
[10 MHz; 450 MHz]	10 <i>V</i>	27.5.3	

In the case of bipolar measurements, the test signal amplitudes are reduced by a factor of 10.



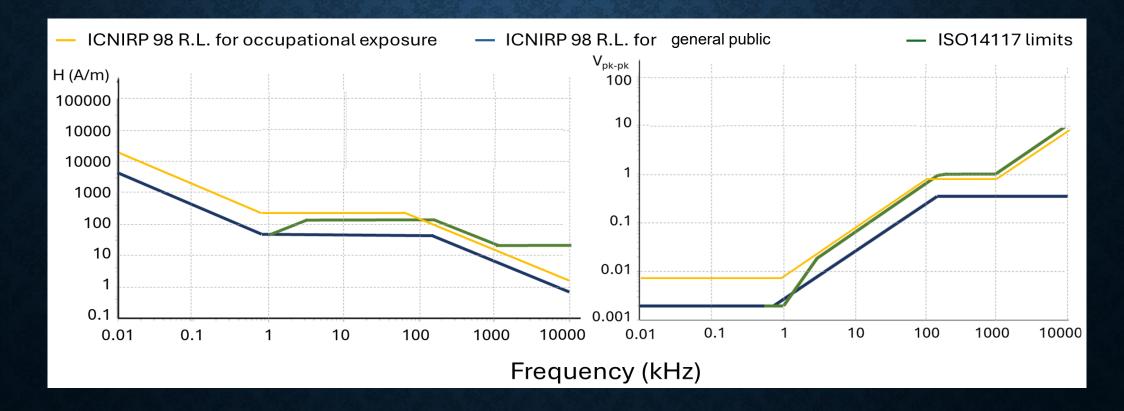
In the EU, the EMC requirements for AIMDs are provided in the standards of the family EN45502. As for pacemaker and implantable cardioverter defibrillators, EMC requirements are provided in the ISO 14117:2019 - Active implantable medical devices — Electromagnetic compatibility — EMC test protocols for implantable cardiac pacemakers, implantable cardioverter defibrillators, and cardiac resynchronization devices.

Standards' background: the immunity levels are determined to protect the AIMD from the foreseeable electromagnetic environment derived from the European Recommendation 1999/519/EC, which was based on the recommendations for the General Public of the ICNIRP Guidelines 1998.



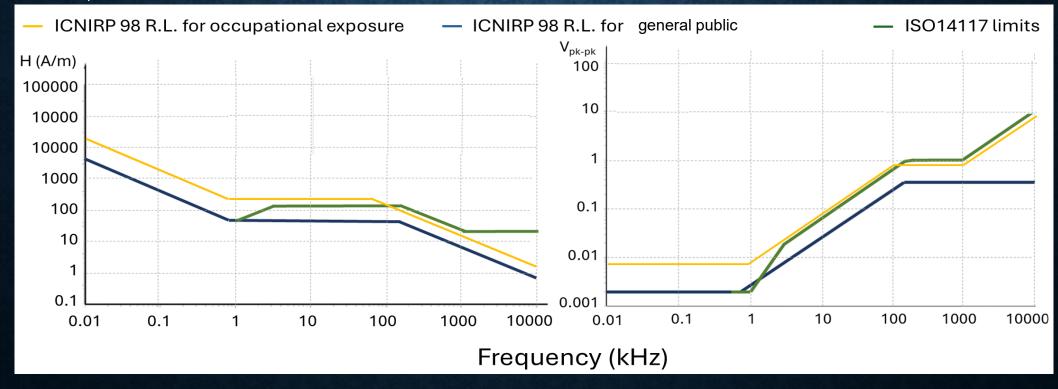
Comparison between the immunity test level adopted by ISO 14117 and ICNIRP 1998 reference level for the general public and occupational exposure (10 Hz to 10 MHz).

The risks for a worker who wears an AIMD could be considered acceptable if exposed to EMF levels below the ICNIRP reference levels for the General Public.





In workplaces, powerful sources of EMF are likely to be encountered, and reference levels for the General Public can be exceeded. Thus, the safety of a worker who wears an AIMD is not guaranteed anymore. In addition, the aforementioned standards take into account only the EMF sources that can be encountered in common-life scenarios (e.g., LTE/4G cellular phones, Wi-Fi transmitters, etc.).





The EMF sources in a work environment can be very specific in terms of modulation, pulse repetition time, etc., and can pose a risk even at levels below the ICNIRP reference levels for the General Public.

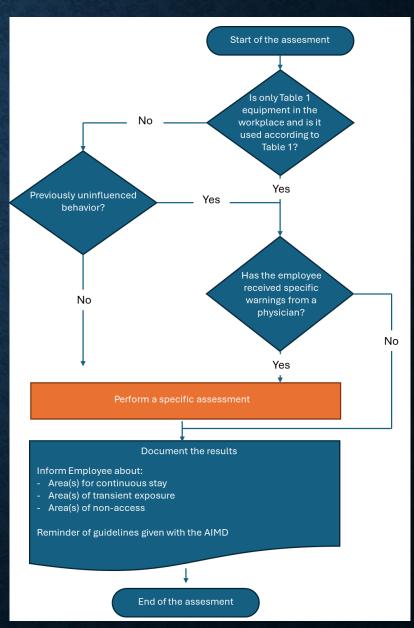
Consequently, the existing standards reasonably protect the General Public wearing AIMDs but are not sufficient to protect workers wearing AIMDs. For these reasons, the EU has developed a series of technical standards to support the employers in the risk assessment of workers who wear AIMDs: the general standard EN50527-1 with the particular standards EN50527-2-X for the different AIMD classes.



RISK ASSESSMENT FOR WORKERS

WITH AIMD

The EN EN50527 family standards provide a general procedure for the specific assessment required for workers with an AIMD: an initial simplified analysis is required, followed, when necessary, by a deeper specific risk assessment for the AIMD-employee.

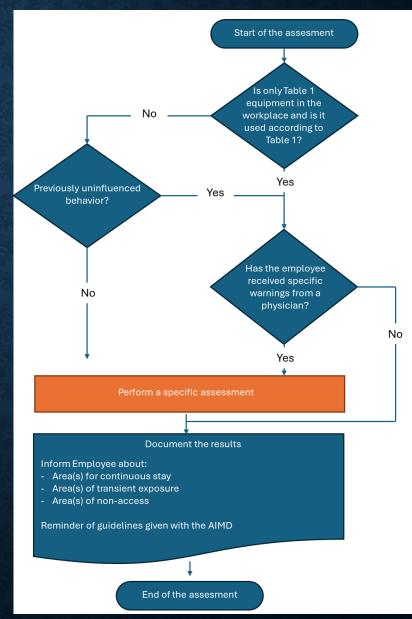




The initial simplified analysis starts from the identification of all the EMF sources active in the workplace and their comparison with a list of equipment reported in a table, called whitelist.

The simplified analysis can be considered sufficient if:

- all the EMF sources are listed in the table;
- all the EMF sources are used in accordance with the indication reported in the "exceptions and remarks" column;
- the AIMD employee has not received specific warnings from the responsible physician that the AIMD may be susceptible to EMI from one of the present equipment.



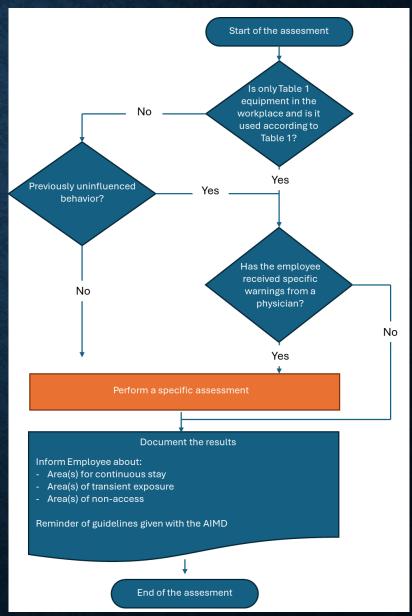


RISK ASSESSMENT FOR WORKERS

WITH AIMD

If one of the previously mentioned conditions is not verified, a specific risk assessment shall be carried out, under the specifications provided in Annex A of the standards. The risk assessment should involve input from:

- 1. the employer and, if applicable, his/her occupational health and safety expert and/or occupational physician;
- 2. the AIMD employee and his/her responsible physician; and
- 3. experts (technical and medical), e.g., the manufacturer of the AIMD.





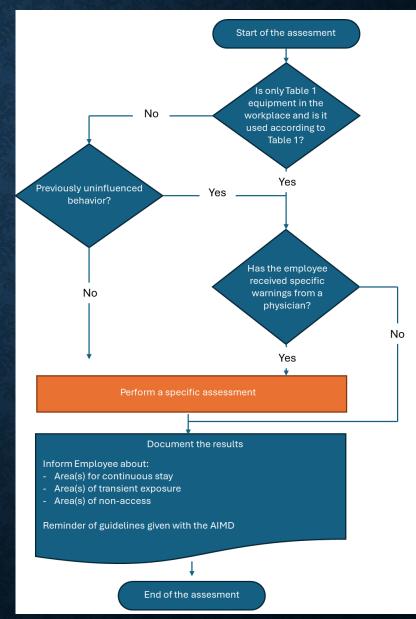
RISK ASSESSMENT FOR WORKERS

WITH AIMD

Then, two alternative methods to perform the risk assessment are proposed: the "non-clinical approach" and the "clinical approach".

The former bases risk assessment on measurement, calculation, and/or information provided by the manufacturer of the AIMD and does not involve the worker directly.

The latter needs the AIMD employee to be exposed under clinical supervision to the foreseeable exposure situations or in a laboratory simulating the workplace exposure situation.





THE AIMD SECTION OF WEBNIR

The guided procedure implemented on the WebNIR platform for risk assessment for workers with AIMDs follows the steps indicated in the technical standard 50527-1, as described previously.

As a first step, after having entered the details of the AIMDs present in the examined worker, the user must indicate whether, in the workplace, there are certain sources of electromagnetic fields, chosen from a preestablished list (the whitelist), indicating for each of these the compliance with the instructions provided in it.

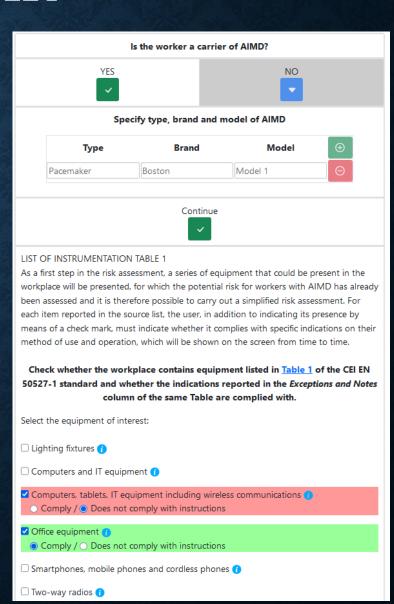
	Is the worker a carrier of AIMD?							
	YES			NO V				
	Specify type, brand and model of AIMD							
	Type Brand			Model	$\boxed{\ \oplus\ }$			
	Pacemaker	Boston	Boston Model 1		$\Big[\ \ominus \ \Big]$			
Continue								
LIST OF INSTRUMENTATION TABLE 1 As a first step in the risk assessment, a series of equipment that could be present in the workplace will be presented, for which the potential risk for workers with AIMD has already been assessed and it is therefore possible to carry out a simplified risk assessment. For each item reported in the source list, the user, in addition to indicating its presence by means of a check mark, must indicate whether it complies with specific indications on their method of use and operation, which will be shown on the screen from time to time. Check whether the workplace contains equipment listed in Table 1 of the CEI EN 50527-1 standard and whether the indications reported in the Exceptions and Notes								
		of the same Tabl	e are con	nplied with.				
Select the equipment of interest:								
Lighting fixtures (1)								
Computers and IT equipment ()								
	 ✓ Computers, tablets, IT equipment including wireless communications ○ Comply / Ooes not comply with instructions 							
✓ Office equipment O Comply / O Does not comply with instructions								
☐ Smartphones, mobile phones and cordless phones ()								



THE AIMD SECTION OF WEBNIR

For such sources, the potential risk for workers with AIMDs has already been assessed, and it is therefore possible to carry out a simplified risk assessment.

The user will then be asked to indicate the presence of other sources not listed in the table, and he will finally be presented with a series of questions relating to the work environment and the clinical history of the worker for whom the risk assessment has to be performed. The procedure will conclude with creating a report summarizing the outcome of the risk assessment procedure.





THANKS